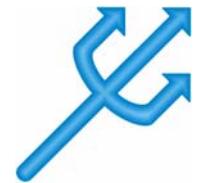


Transparency: Shedding Light on PA Modeling

John Tauxe



Neptune and Company



Presentation Topics

Transparency is important in...

- Coding
- User Interface
- Communicating Concepts
- Documentation
- Decision Making



Transparency in Coding

This is opaque code:

```
FUNCTION BESSI(N,X)
  PARAMETER(IACC=40,BIGNO=1.0E10,BIGNI=1.0E-10)
  IF (N.LT.2) PAUSE 'bad argument N in BESSI'
  TOX=2.0/X
  BIP=0.0
  BI=1.0
  BESSI=0.
  M=2*((N+INT(SQRT(FLOAT(IACC*N)))))  
DO 11 J=M,1,-1
    BIM=BIP+FLOAT(J)*TOX*BI
    BIP=BI
    BI=BIM
    IF (ABS(BI).GT.BIGNO) THEN
      BESSI=BESSI*BIGNI
      BI=BI*BIGNI
      BIP=BIP*BIGNI
    ENDIF
    IF (J.EQ.N) BESSI=BIP
11  CONTINUE
  BESSI=BESSI*BESSIO(X)/BI
  RETURN
END
```

```
#include <math.h>
#define ACC 40.0
#define BIGNO 1.0e10
#define BIGNI 1.0e-10
float bessi(n,x)
int n;
float x;
{
  int j;
  float bi,bim,bip,tox,ans;
  float bessi0();
  void nrerror();
  if (n < 2) nrerror("Index n less than 2 in BESSI");
  if (x == 0.0)
    return 0.0;
  else {
    tox=2.0/fabs(x);
    bip=ans=0.0;
    bi=1.0;
    for (j=2*(n+(int) sqrt(ACC*n));j>0;j--) {
      bim=bip+j*tox*bi;
      bip=bi;
      bi=bim;
      if (fabs(bi) > BIGNO) {
        ans *= BIGNI;
        bi *= BIGNI;
        bip *= BIGNI;
      }
      if (j == n) ans=bip;
    }
    ans *= bessi0(x)/bi;
    return x < 0.0 && n%2 == 1 ? -ans : ans;
  }
}
#undef ACC
#undef BIGNO
#undef BIGNI
```

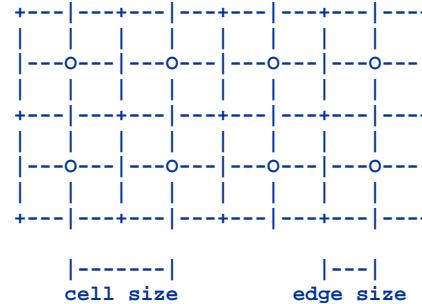
with apologies to *Numerical Recipes*

Transparency in Coding

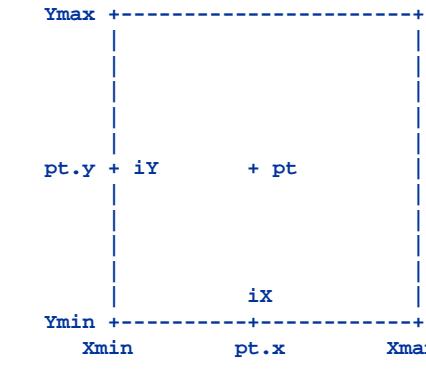
This is commented code: Remember ASCII art?

```
{  
    /* dfWinbox and dfCellSize are defined globally */  
    double dfX, dfY;           /* f.p. index to cell */  
    double dfDenominator;      /* temp variable */  
    int iX, iY;                /* cell index number */  
    int nxLower, nyLower;       /* index to lower bounding cell */  
    int nxUpper, nyUpper;       /* index to upper bounding cell */  
    POINT ptLower, ptUpper;     /* corner points bounding cell */  
    float fTemp;               /* temporary variable */  
  
    /* I was forced to add this since for some reason nCols and nRows  
     * are not consistently read properly above using PrivateWindowCols  
     * and PrivateWindowCols. */  
    nCols = (int)( ( Xmax( dfWinbox ) - Xmin( dfWinbox ) ) / dfCellSize );  
    nRows = (int)( ( Ymax( dfWinbox ) - Ymin( dfWinbox ) ) / dfCellSize );  
  
    /* Determine which cell contains the point ppt. */  
    /* First, work with the GRID cells, to subdivide later. */  
  
    /* Find cell index number of Lower bounding cell. */  
    dfX = ( ppt->x - Xmin( dfWinbox ) ) / dfCellSize;  
    iX = (int)dfX;             /* truncation to integer */  
  
    dfY = ( Ymax( dfWinbox ) - ppt->y ) / dfCellSize;  
    iY = (int)dfY;             /* truncation to integer */  
  
    pcell->iX = iX;  
    pcell->iY = iY;  
}
```

* So for the purposes of this DarcyTrack function, the elemental
* cell over which calculations are done must be a quarter
of the original GRID cells, to ensure uniform properties
over the cell area:



Notes on orientation: (This is a square GRID cell)



pt.x and pt.y are in real coordinates

Xmin, Xmax, Ymin, Ymax are in real coordinates, and are the limits of the grid, as stored in the global variable dfWinbox

ix and iy are cell column (left to right) and row (top to bottom)



Transparency in the User Interface

Old school UI design: Text

```

A sample parameter file.
0
30
100    C:\>
0      C:\>EDIT MODEL.DAT
4      C:\>RUN MODEL.EXE
C:\>TYPE MODEL.OUT

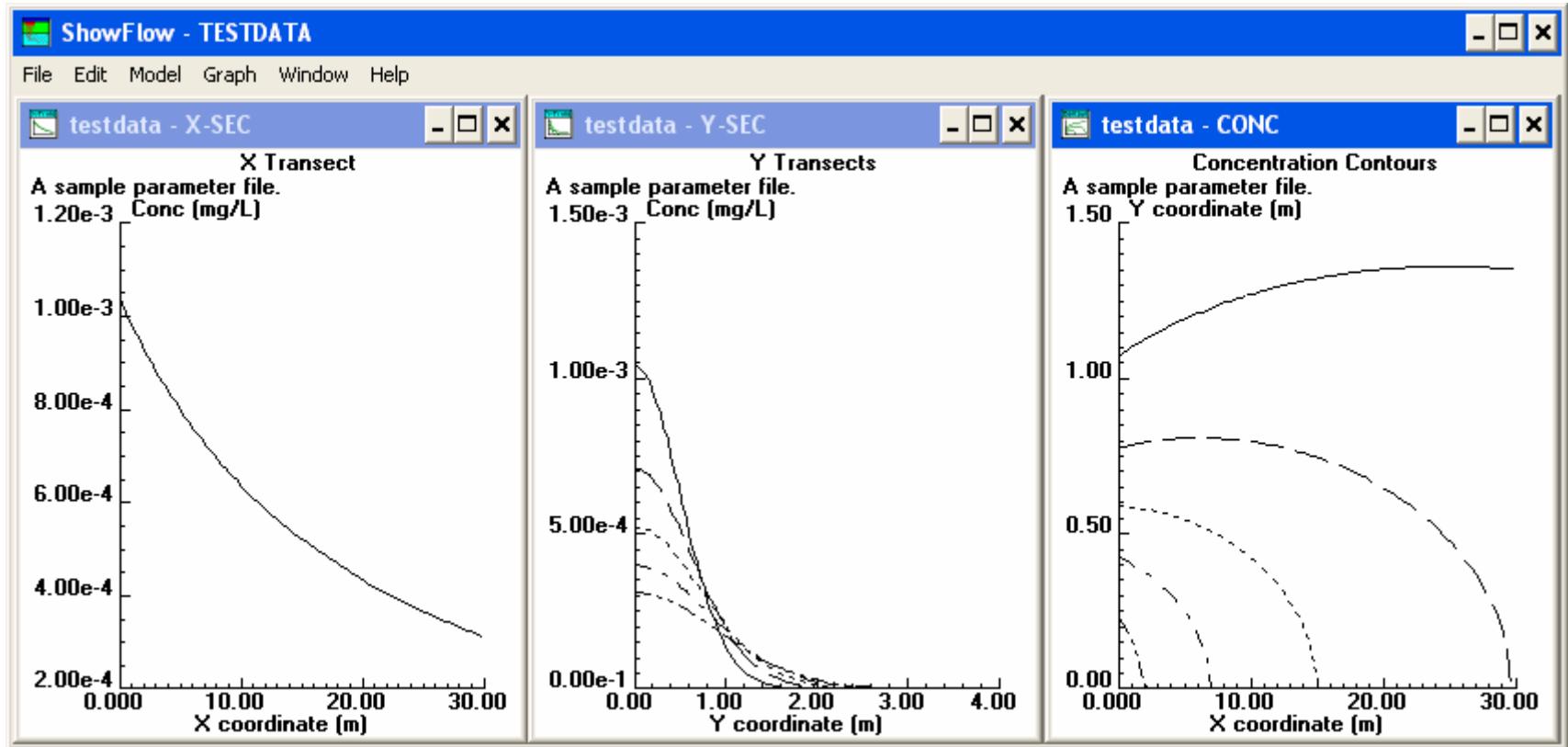
100
2      0.00E+000 1.07E+000 7.76E-001 5.89E-001 4.22E-001 2.30E-001
10     5.05E-001 1.09E+000 7.81E-001 5.87E-001 4.12E-001 1.98E-001
1      1.01E+000 1.10E+000 7.91E-001 5.82E-001 3.88E-001 1.02E-001
1.52E+000 1.11E+000 7.91E-001 5.85E-001 4.01E-001 1.59E-001
2      2.02E+000 1.13E+000 7.94E-001 5.79E-001 3.75E-001 0.00E+000
2.53E+000 1.14E+000 7.98E-001 5.75E-001 3.59E-001 0.00E+000
3      3.03E+000 1.15E+000 8.01E-001 5.70E-001 3.42E-001 0.00E+000
3.54E+000 1.16E+000 8.03E-001 5.65E-001 3.22E-001 0.00E+000
4      4.04E+000 1.17E+000 8.05E-001 5.58E-001 3.00E-001 0.00E+000
4.55E+000 1.18E+000 8.07E-001 5.52E-001 2.76E-001 0.00E+000
5      5.05E+000 1.19E+000 8.08E-001 5.44E-001 2.47E-001 0.00E+000
5.56E+000 1.20E+000 8.08E-001 5.36E-001 2.13E-001 0.00E+000
6      6.06E+000 1.21E+000 8.09E-001 5.26E-001 1.79E-001 0.00E+000
6.57E+000 1.22E+000 8.09E-001 5.17E-001 1.09E-001 0.00E+000
7      7.07E+000 1.23E+000 8.08E-001 5.06E-001 0.00E+000 0.00E+000
7.58E+000 1.24E+000 8.07E-001 4.94E-001 0.00E+000 0.00E+000
8      8.08E+000 1.24E+000 8.06E-001 4.81E-001 0.00E+000 0.00E+000
8.59E+000 1.25E+000 8.04E-001 4.68E-001 0.00E+000 0.00E+000
9      9.09E+000 1.26E+000 8.02E-001 4.53E-001 0.00E+000 0.00E+000
9.60E+000 1.27E+000 7.99E-001 4.37E-001 0.00E+000 0.00E+000
10     1.01E+001 1.27E+000 7.96E-001 4.20E-001 0.00E+000 0.00E+000
11     1.06E+001 1.28E+000 7.93E-001 4.01E-001 0.00E+000 0.00E+000
12     1.11E+001 1.28E+000 7.89E-001 3.80E-001 0.00E+000 0.00E+000
13     1.16E+001 1.29E+000 7.85E-001 3.57E-001 0.00E+000 0.00E+000
14     1.21E+001 1.30E+000 7.80E-001 3.32E-001 0.00E+000 0.00E+000
15     1.26E+001 1.30E+000 7.75E-001 3.04E-001 0.00E+000 0.00E+000
16     1.31E+001 1.31E+000 7.70E-001 2.72E-001 0.00E+000 0.00E+000
17     1.36E+001 1.31E+000 7.64E-001 2.34E-001 0.00E+000 0.00E+000
18     1.41E+001 1.32E+000 7.57E-001 1.87E-001 0.00E+000 0.00E+000

```



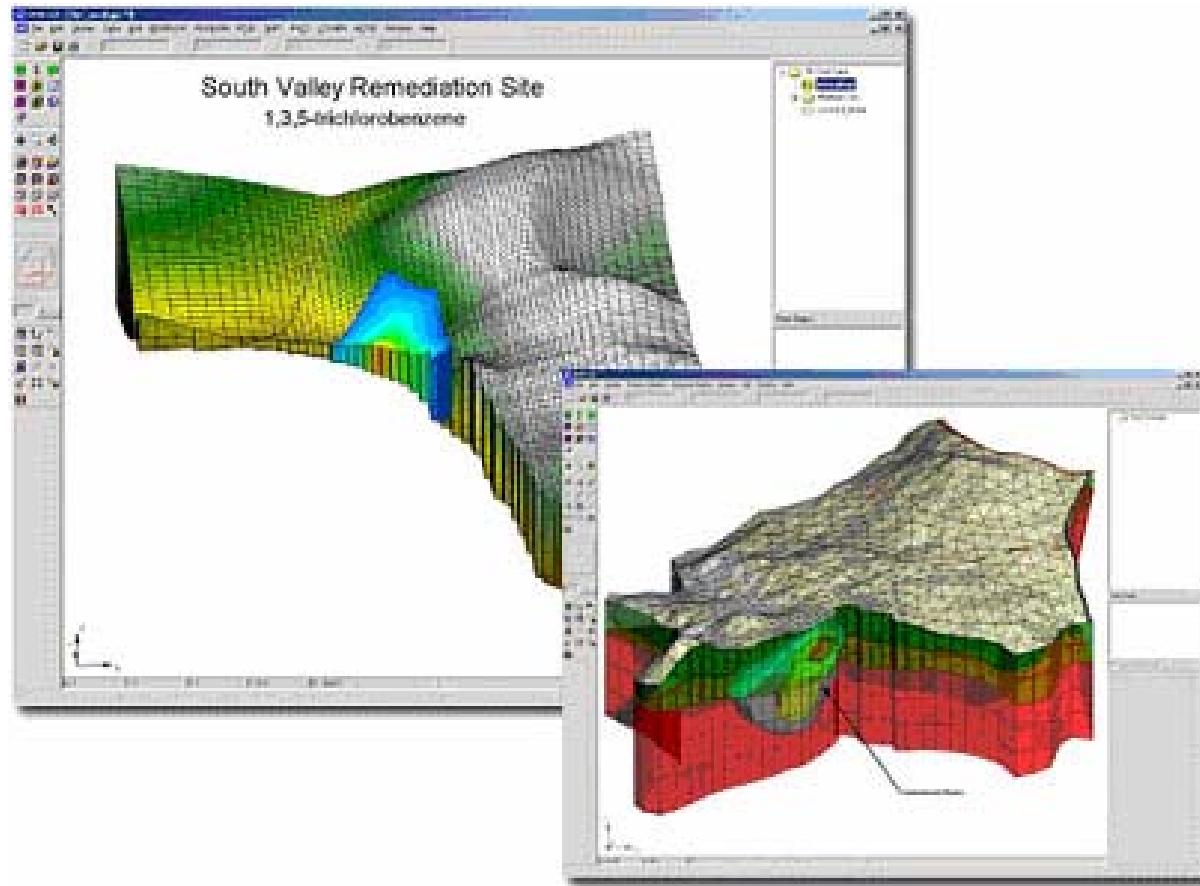
Transparency in the User Interface

Better UI design: Graphical forms and output



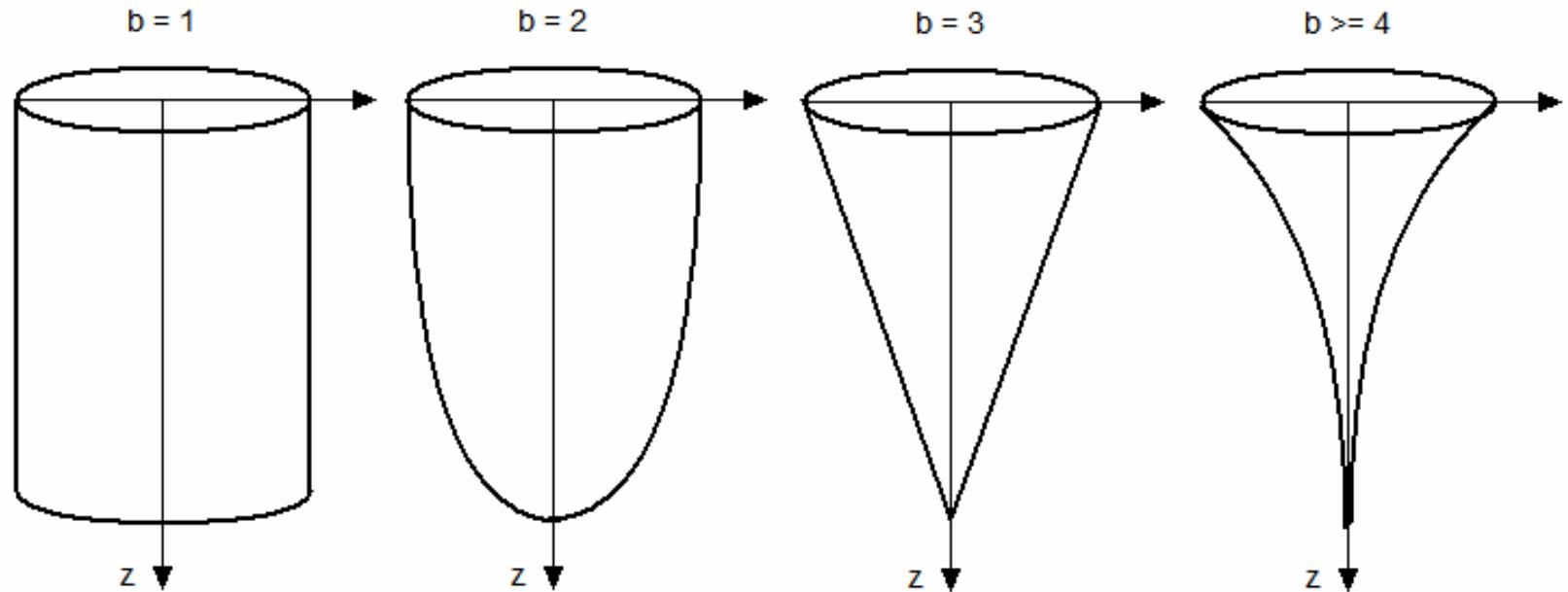
Transparency in the User Interface

Even better UI design: Interactive tools



Transparency in Concepts

The shape of root masses (or burrows) underground is shown here for various values of b :

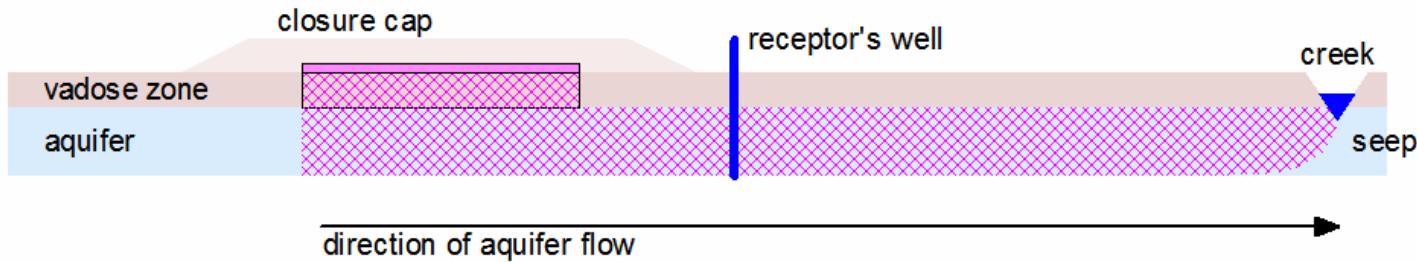


A simple illustration can aid explanation



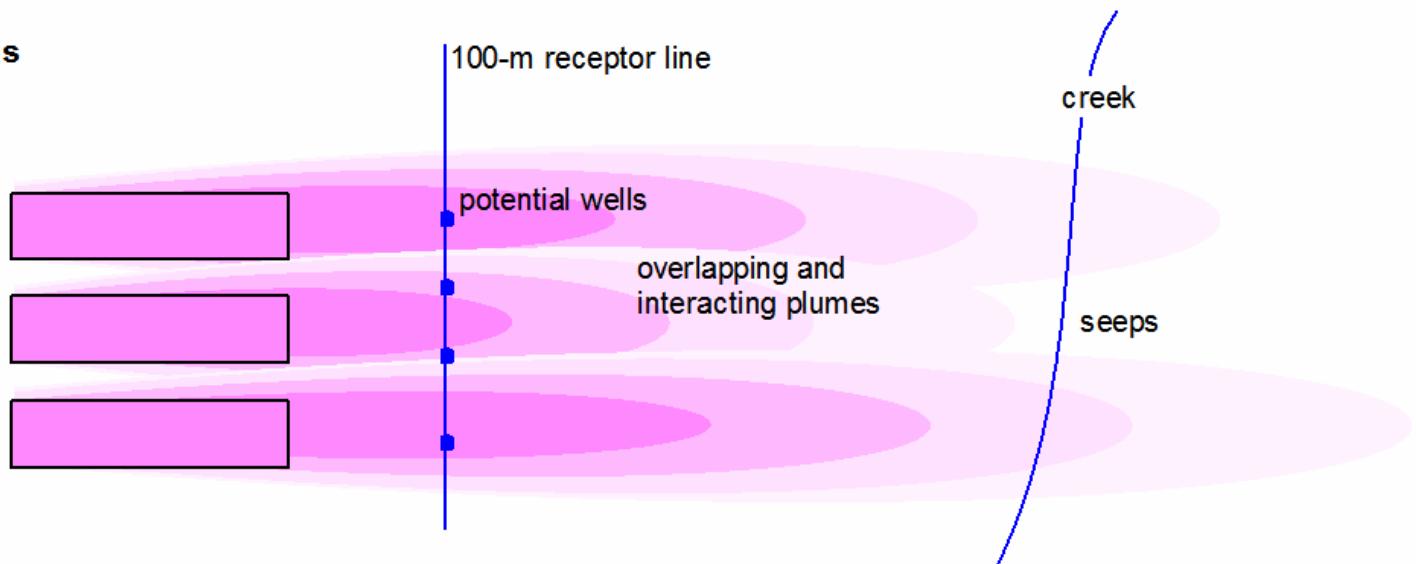
Transparency in Concepts

Elevation



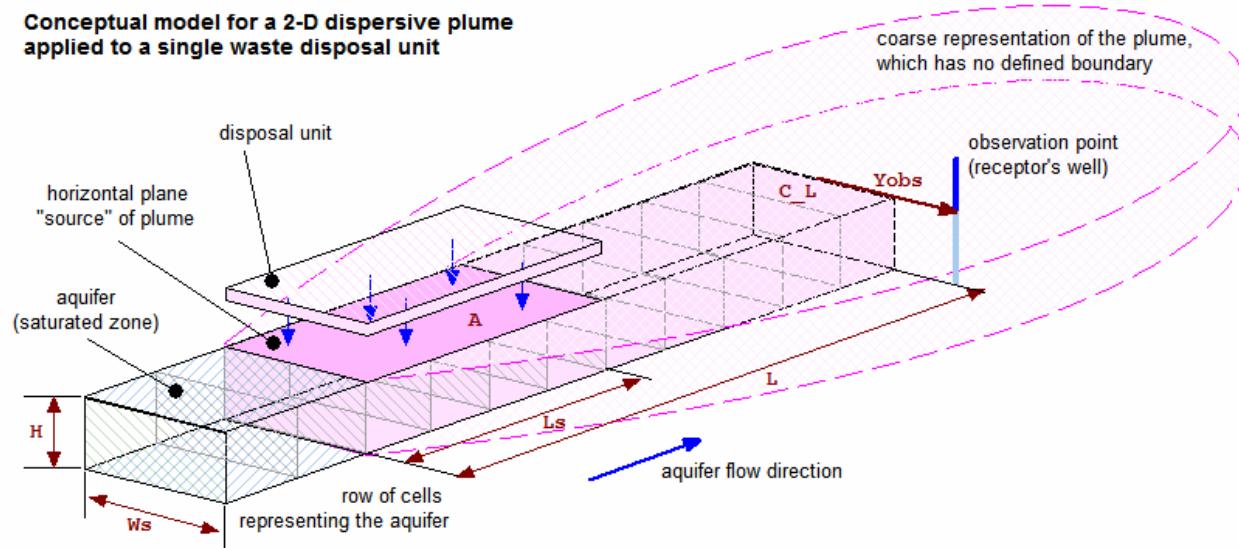
Plan View

Multiple Trench Units



Transparency in Concepts

Modeling tools can be described



Application of the GoldSim Plume Function

As described in the GoldSim on-line help (search for "plume"), the plume() function accepts 11 arguments. The description presented here is somewhat simplified for the case at hand. The arguments to the function are as follows, with comments following the "//". Footnotes are below.

```
plume (
    L,           // length of the Pipe or row of Cells, as measured from
                // the upstream end of the Source1
    A,           // cross-sectional area of the Pipe or Cells
    Ls,          // length of the Source set equal to the length of the
                // overlying disposal unit, parallel to flow
    0,           // vertical offset of observation point (zero)2
```

Transparency in Concepts

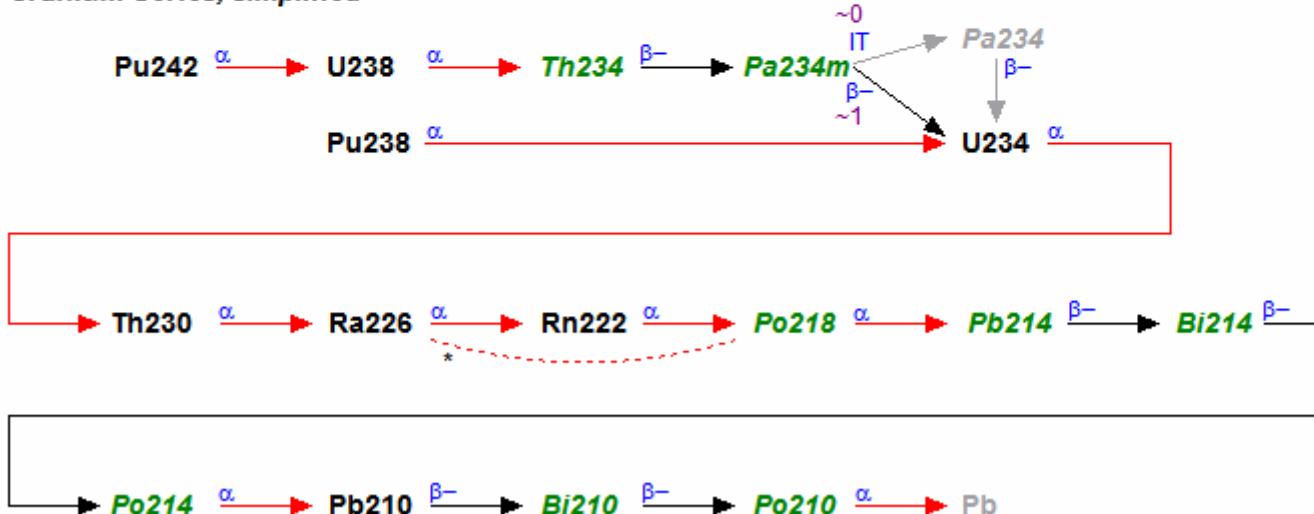
Decay chains implemented in contaminant transport and dose calculations

Note that the radionuclides and stable nuclides in black are maintained in the Species list. Any modification to the decay chain diagram needs to have an associated modification to the Species list, and vice versa.

The radionuclides noted in green italic are considered in the dose assessment only, through dose conversion factors. Environmental transport of these progeny is assumed to follow their respective parents, with which they are in secular equilibrium.

Radionuclides, stable nuclides, and decay arrows in gray are not represented in the model, but are shown here for completeness.

Uranium Series, simplified



* Rn222 is partially bypassed in proportion to account for partial emanation.



Transparency in Documentation

Models should be ...

- readable,
- traceable,
- supported, and
- *informative*.

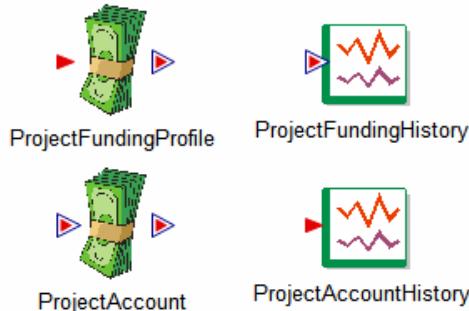


Readability

Project budget and accounting

The user can specify the funding profile, which constitutes annual increases to the project account. Costs are deducted from the project account as tasks start and complete.

Main Project Account

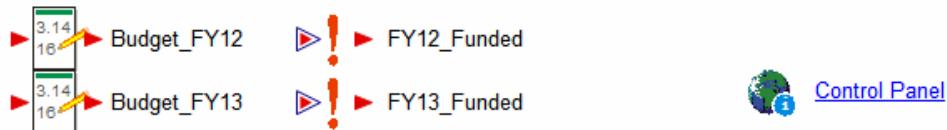


The ProjectAccount has revenues added each FY, as worked out above.

It also has these deductions:

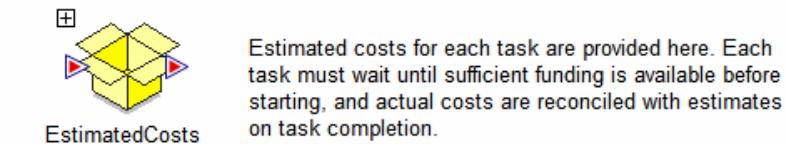
- each task deducts its estimated cost on task start
- each task reconciles its actual costs with the estimated cost, and deducts the difference on completion of the task
- penalties and fines are deducted as they occur

Funding Profile (set on Control Panel)

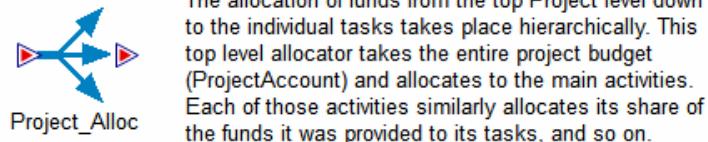


[Control Panel](#)

Estimated expenses and allocation priorities



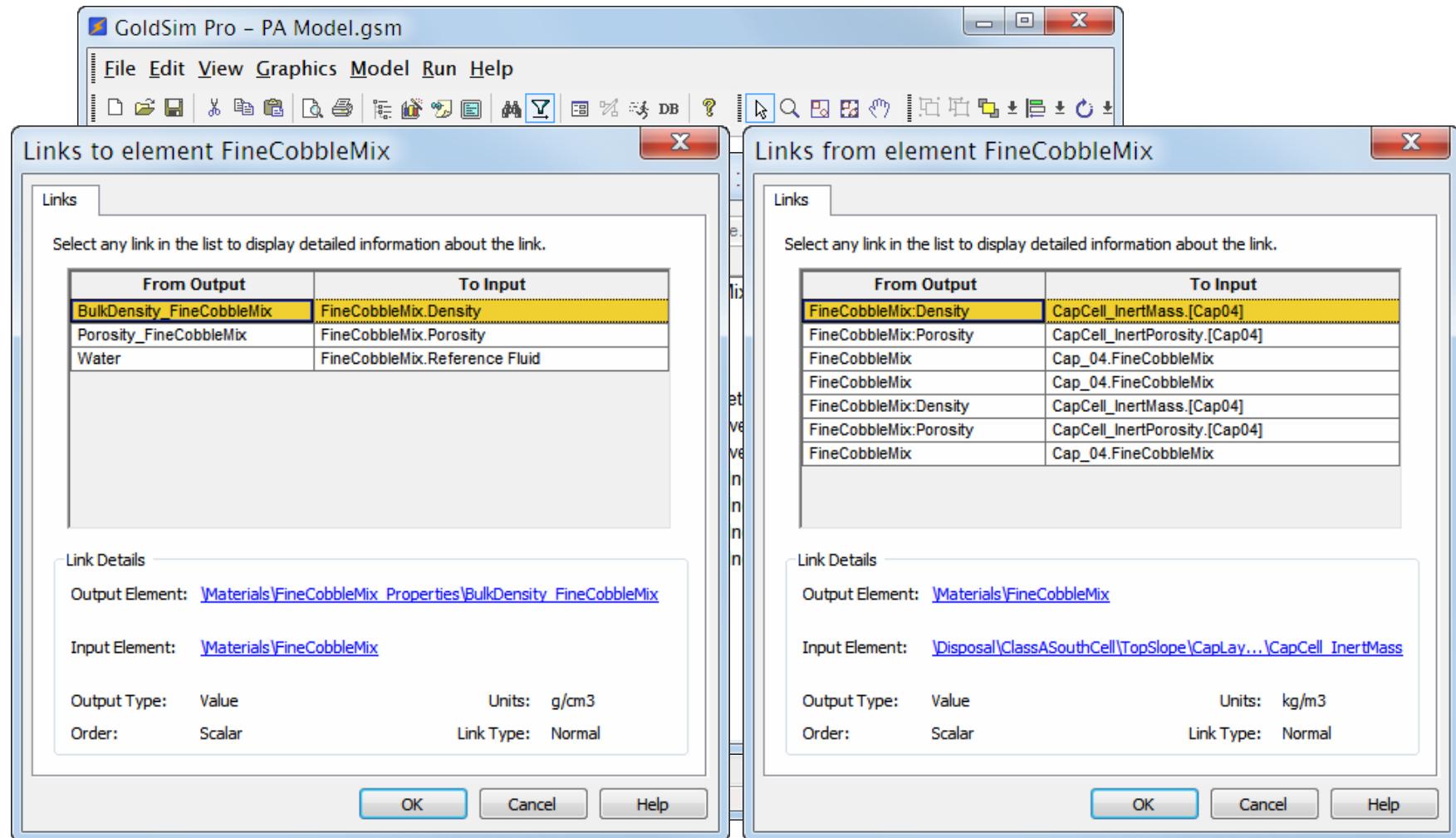
Funding allocations are determined as annual spending rates.



- [Waste Characterization Funding](#)
- [Public Involvement Funding](#)
- [Operations Funding](#)
- [Compliance Activities Funding](#)
- [Public Involvement Activities Funding](#)



Traceability Within the Model



Traceability Outside the Model

TABLE 7. HELP INFILTRATION MODEL LAYERS AND MATERIAL PROPERTIES

| Layer | Material | Thickness (inches) | n (vol/vol) | θ_{fc} (vol/vol) | θ_{wp} (vol/vol) | Available Moisture (vol/vol) | θ_i (vol/vol) | K_s (cm/sec) | Layer Type | Size Range (inches) | Material Description | Notes: |
|---------|-----------------------|--------------------|-------------|-------------------------|-------------------------|------------------------------|----------------------|----------------|----------------------|---------------------|---------------------------|--|
| Layer 1 | Type-B Rip Rap | 18 | 0.190 | 0.024 | 0.007 | 0.017 | initialized to ss | 42 | vertical percolation | 0.75-4.5 | 1.25 inches | Size is nominal diameter |
| Layer 2 | Type-A Filter (upper) | 6 | 0.190 | 0.024 | 0.007 | 0.017 | initialized to ss | 42 | vertical percolation | 0.08-6.0 | Coarse Sand - Fine Cobble | |
| Layer 3 | Sacrificial Soil | 12 | 0.31 | 0.2 | 0.025 | 0.175 | initialized to ss | 4.00E-03 | vertical percolation | <0.75 | Silty Sand and Gravel | Placed at 4×10^{-4} cm/sec; freeze/thaw reduces K to 4×10^{-3} cm/sec. |
| Layer 4 | Type-B Filter (lower) | 6 | 0.28 | 0.032 | 0.013 | 0.019 | initialized to ss | 3.5 | lateral drainage | 0.2-1.5 | Coarse Sand - Fine Gravel | |
| Layer 5 | Upper Radon Barrier | 12 | 0.430 | 0.390 | 0.28 | 0.11 | 0.43 | 5.00E-08 | barrier soil | n/a | Clay | |
| Layer 6 | Lower Radon Barrier | 72 | 0.430 | 0.390 | 0.28 | 0.11 | 0.39 | 1.00E-06 | vertical percolation | n/a | Clay | |
| Layer 7 | Waste | 100 | 0.437 | 0.062 | 0.024 | 0.038 | initialized to ss | 5.00E-04 | vertical percolation | n/a | Sand | Unit thickness for waste. Model is insensitive to waste thickness variation. |
| Layer 8 | Clay Liner | 24 | 0.430 | 0.390 | 0.28 | 0.11 | 0.43 | 1.00E-06 | barrier soil | n/a | Clay | |

n = Porosity

θ_{fc} = Field Capacity

θ_{wp} = Wilting Point

θ_i = Initial Moisture Content

K_s = Saturated Hydraulic Conductivity

θ_i = Value for initialized steady-state moisture content are given in the model output files.

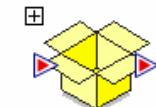
Available Moisture: = Moisture available to be evaporated is only applicable in the upper 18 inches of the model

Engineered material properties

Engineered materials are in a variety of forms serving various purposes. These are used in the construction of the cap (top slope and side slope) and liner layers.



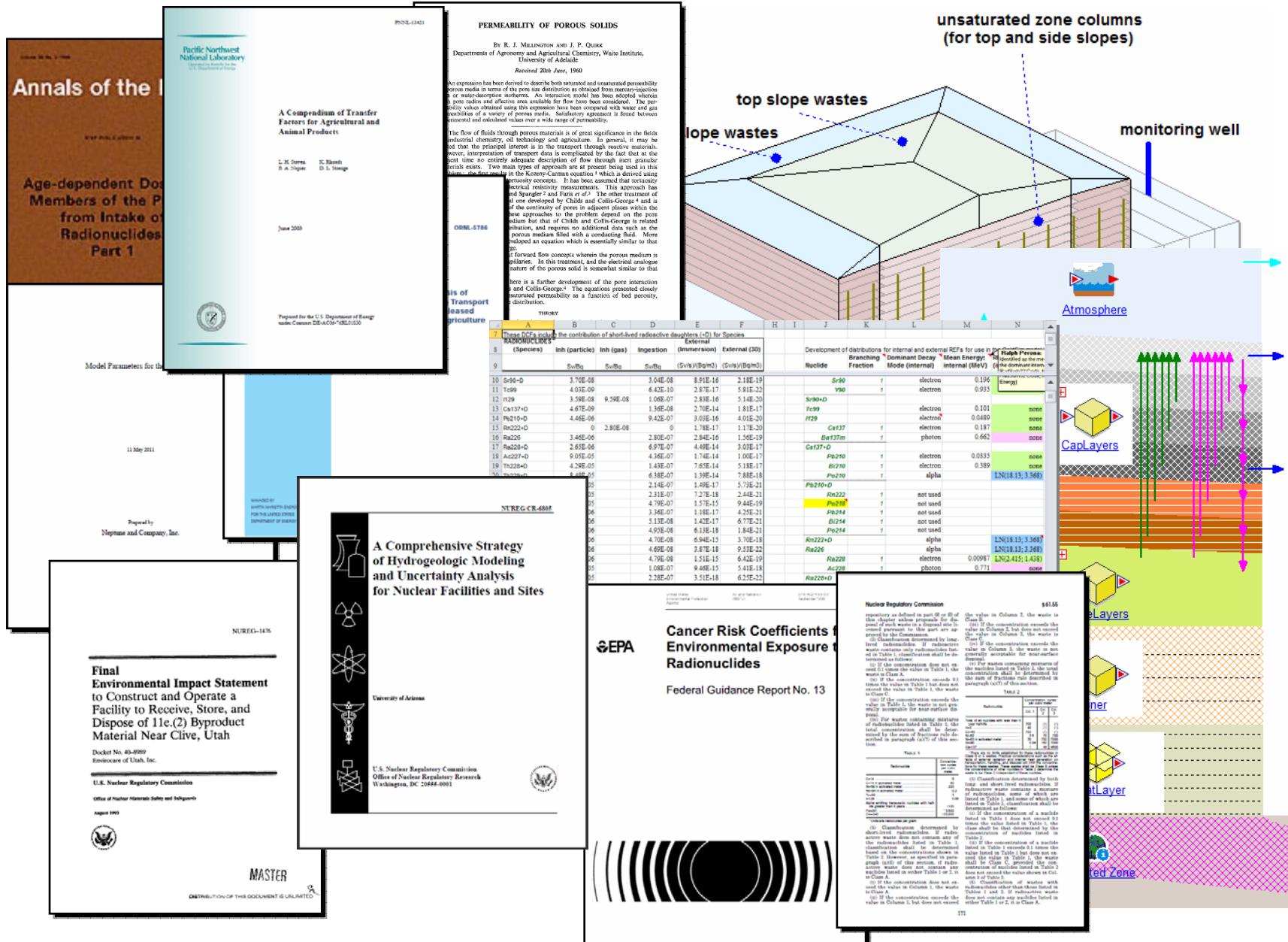
RipRap



RipRap_Properties

Rip Rap is used to construct the uppermost layer: Armor. It quickly becomes infilled with Loess. The Rip Rap itself is assumed to be an inert material.





Bringing it Together

Radon flux estimates according to NRC Uranium Mill Tailings Cover Guidance

These radon flux calculations are based in the U.S. Nuclear Regulatory Commission Regulatory Guide 3.64, "Calculation of Radon Flux Attenuation by Earthen Uranium Mill Tailings Covers" (NRC 1989), and NUREG/CR-3533, "Radon Flux Calculations for Uranium Mill Tailings Cover Design" (NRC 1984). Since all embankment cover designs are quite similar, the calculation is performed only for the TopSlope of the Class A South embankment, and is applied to other slopes.

The calculation proceeds from the bottom up (waste to surface), as outlined on page 14 and Example 2 in Appendix A of NRC (1989). First is calculated a flux from the DU waste itself, assuming no overlying barrier. That flux is used as an input boundary condition for the subsequent calculation, which estimates the flux



A graphical summary of the flux results through each stage is provided here.

RefFluxGraph_TS

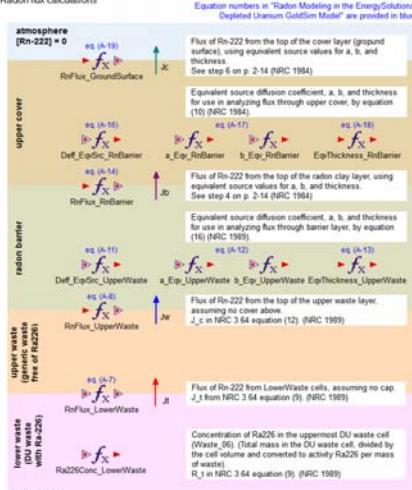
Background calculations:

The layers that this radon diffusion calculation considers are:
 • near-surface soils (all cover materials above the clay)
 • compacted clay radon barrier
 • sandstone (with no radon parent) - similar to soil (UpperWaste)
 • DU waste containing radon parents (LowerWaste)

The bottommost layer has a radon-226 concentration that drives the radon production.
 All layers have the following background calculations, defined below:
 • thickness (meters and deposited mass per unit area)
 • relaxation length b, from NRC 3.64 eq. (11)
 • inverse relaxation length b, from NRC 3.64 eq. (10)

| layer thickness | interface constant | inverse relaxation length |
|----------------------------|----------------------------------|----------------------------------|
| f_X Cover_Thickness | $f_X \rightarrow a_{Cover}$ | $f_X \rightarrow b_{Cover}$ |
| f_X RadBamer_Thickness | $f_X \rightarrow a_{RadBamer}$ | $f_X \rightarrow b_{RadBamer}$ |
| f_X UpperWaste_Thickness | $f_X \rightarrow a_{UpperWaste}$ | $f_X \rightarrow b_{UpperWaste}$ |
| f_X LowerWaste_Thickness | $f_X \rightarrow a_{LowerWaste}$ | $f_X \rightarrow b_{LowerWaste}$ |

Radon flux calculations



NOT TO SCALE

Radon

U.S. NUCLEAR REGULATORY COMMISSION

June 1989

REGULATORY GUIDE

OFFICE OF NUCLEAR REGULATORY RESEARCH

The "O" "N" all Cl Th Ap Th

REGULATORY GUIDE 3.64
(Task WM 503-4)

CALCULATION OF RADON FLUX ATTENUATION BY EARTHEN URANIUM MILL TAILINGS COVERS

over Guidance

on Regulatory Guide 3.64, NRC 1989), and "Design" (NRC 1984). Since for the TopSlope of the

ge 14 and Example 2 in suming no overlying barrier. which estimates the flux

ough each



Dff for Radon



Radon Flux Calibration



NRC Reg. Guide 3.64



NUREG/CR-3533



GoldSim Model Calculations

NUCLEAR REGULATORY GUIDES

The guides are issued in the following ten broad divisions:

1. Power Reactors
2. Research and Test Reactors
3. Commercial Facilities
4. Environmental and String
5. Materials and Plant Protection
6. Products
7. Transportation
8. Radiation Health
9. Antimun and Financial Review
10. General

Copies of issued guides may be purchased from the Government Printing Office at the current GPO price. Information on current GPO prices may be obtained by writing to the Superintendent of Documents, U.S. Government Printing Office, Post Office Box 37092, Washington, DC 20013-7052, telephone (202)276-2060 or (202)275-2171.

Written comments may be submitted to the Regulatory Publications Branch, DRRS, ARM, U.S. Nuclear Regulatory Commission, Washington, DC 20585.

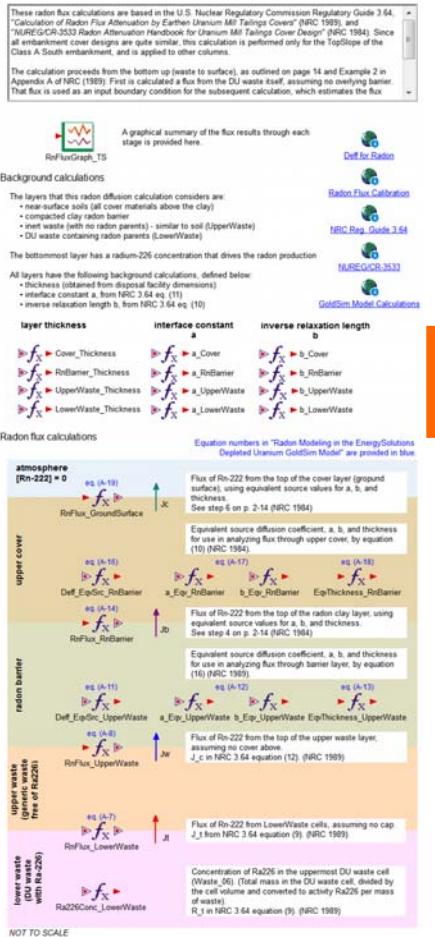
Issued guides may also be purchased from the National Technical Information Service on a standing order basis. Details on this service may be obtained by writing NTIS, 5285 Port Royal Road, Springfield, VA 22161.

Interface constant a, from NRC 3.64 eq. (11)

• inverse relaxation length b, from NRC 3.64 eq. (10)

Bringing it Together

Radon flux estimates according to NRC Uranium Mill Tailings Cover Guidance



layer thickness

- f_X ► Cover_Thickness
- f_X ► RnBarrier_Thickness
- f_X ► UpperWaste_Thickness
- f_X ► LowerWaste_Thickness

interface constant a

- f_X ► a_Cover
- f_X ► a_RnBarrier
- f_X ► a_UpperWaste
- f_X ► a_LowerWaste

inverse relaxation length b

- f_X ► a_Cover
- f_X ► a_RnBarrier
- f_X ► a_UpperWaste
- f_X ► a_LowerWaste

inverse relaxation length b

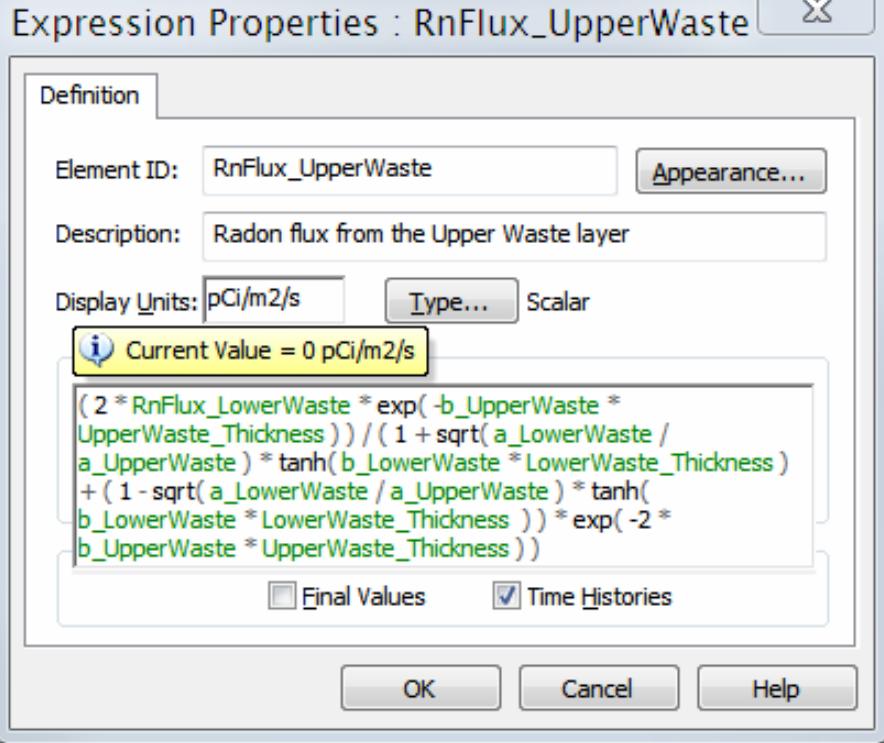
- f_X ► b_Cover
- f_X ► b_RnBarrier
- f_X ► b_UpperWaste
- f_X ► b_LowerWaste

Sometimes simply organizing the appearance of calculations can help in communicating their role.

Bringing it Together

This flux is given by NRC (eq. 3 in NRC, 1984 and eq. 9 in NRC, 1989) as

$$J_t = R_t \rho_t E_t \sqrt{\lambda D_t} \tanh(x_t \sqrt{\lambda/D_t}) \quad (\text{A-7})$$



is used in the second step to solve for the surface flux of radon assuming continuity of continuity of concentration across the tailings-cover interface (eq. 4 in NRC, 1984 and NRC, 1989):

$$J_c = \frac{2 J_t \exp(-b_c x_c)}{1 + \sqrt{\frac{a_t}{a_c}} \tanh(b_t x_t) + \left[1 - \sqrt{\frac{a_t}{a_c}} \tanh(b_t x_t) \right] \exp(-2 b_c x_c)} \quad (\text{A-8})$$

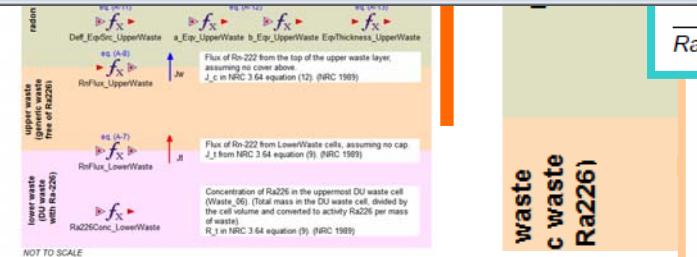
subscript *c* refers to the cover (in this case, the bottommost layer or inert Class A) and the inverse relaxation lengths are defined as

$$b_t = \sqrt{\lambda/D_t} \quad \text{and} \quad b_c = \sqrt{\lambda/D_c} \quad (\text{A-9})$$

NRC, 1989) and the interface constants are defined (eq. 11 in NRC, 1989) as

$$a_t = n_t^2 D_t [1 - (1-k)m_t]^2 \quad \text{and} \quad a_c = n_c^2 D_c [1 - (1-k)m_c]^2 \quad (\text{A-10})$$

equilibrium distribution coefficient for radon in water and air (pCi cm⁻³ water per pCi cm⁻³ air).



Radon Modeling

$$J_c = \frac{2 J_t \exp(-b_c x_c)}{1 + \sqrt{a_t/a_c} \tanh(b_t x_t) + [1 - \sqrt{a_t/a_c} \tanh(b_t x_t)] \exp(-2 b_c x_c)} \quad (12)$$

Transparency in Decision Making

Decision makers include ...

- regulators • site operators

Decision makers must ...

- answer to science,
- answer to the law,
- answer to the public,
- live with uncertainty, and
- sleep at night.

Performance Assessment should help in all these aspects.



Science

$$N_i = \lambda_1 \lambda_2 \cdots \lambda_{i-1} N_{1(0)} \sum_{j=1}^i \frac{e^{-\lambda_j t}}{\prod_{k \neq j} (\lambda_k - \lambda_j)}$$

$$C_{water} = \left(1 + K_d \frac{\rho_b}{\theta_w} \right) \times C_{soil}$$

$$\nu_x = \frac{K}{n} \nabla h$$

$$Q_{atm} = f_R \times C_{soil}$$

$$\tilde{J} = -\theta_w D_s \nabla C$$



Public



Law and Regulation

§ 61.41 Protection of the general population from releases of radioactivity.

Concentrations of radioactive material which may be released to the general environment in ground water, surface water, air, soil, plants, or animals must not result in an annual dose exceeding an equivalent of 25 millirems to the whole body, 75 millirems to the thyroid, and 25 millirems to any other organ of any member of the public. Reasonable effort should be made to maintain releases of radioactivity in effluents to the general environment as low as is reasonably achievable.

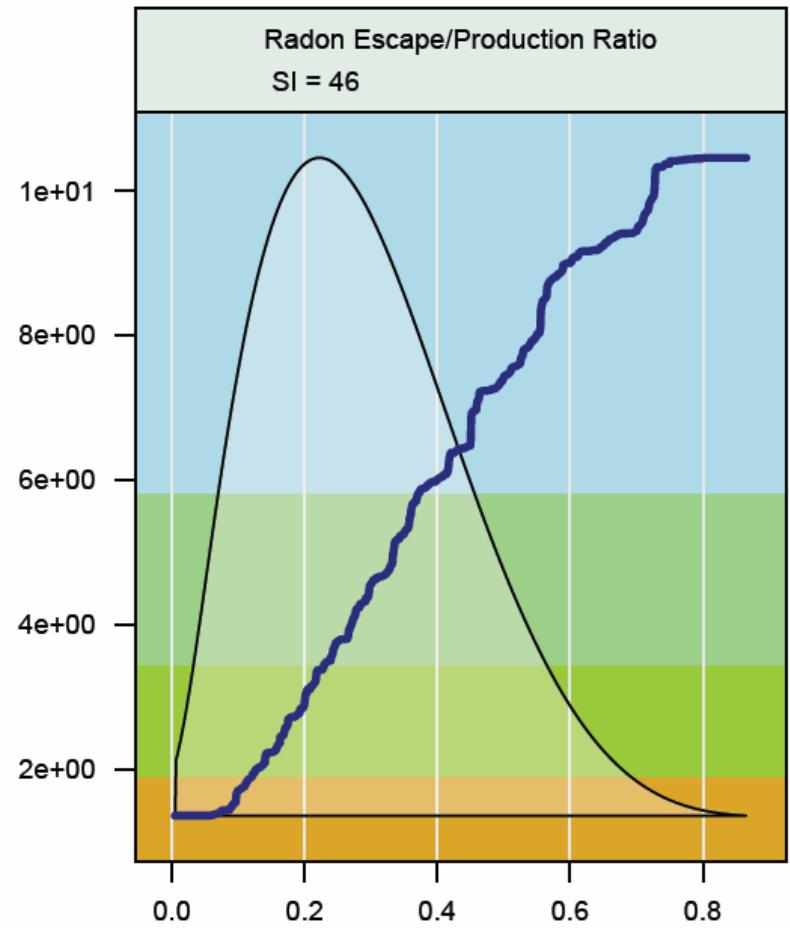
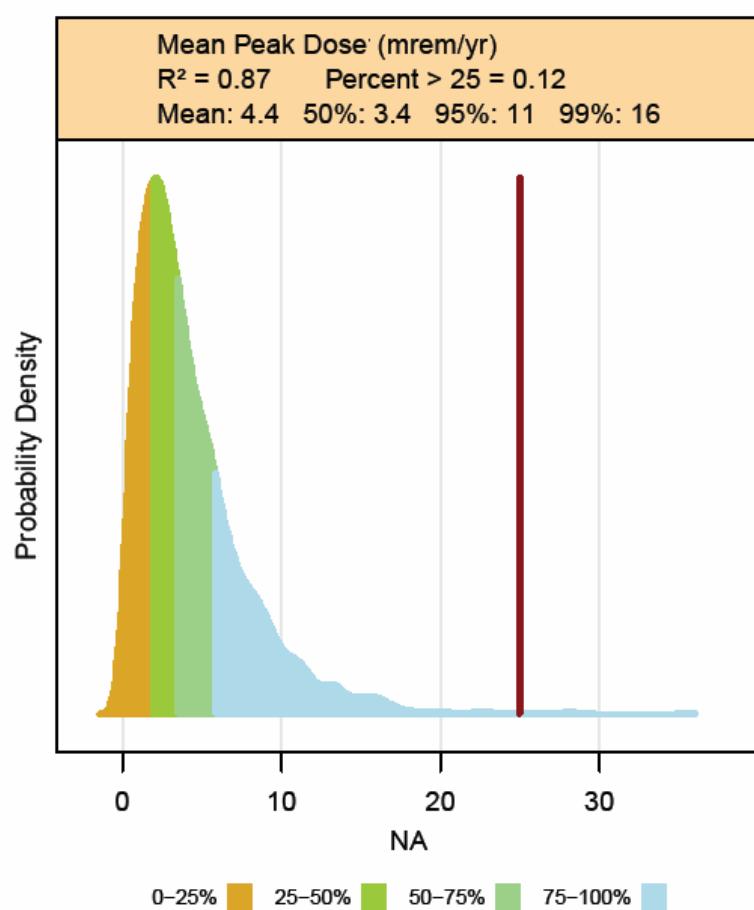
§ 61.42 Protection of individuals from inadvertent intrusion.

Design, operation, and closure of the land disposal facility must ensure protection of any individual inadvertently intruding into the disposal site and occupying the site or contacting the waste at any time after active institutional controls over the disposal site are removed.

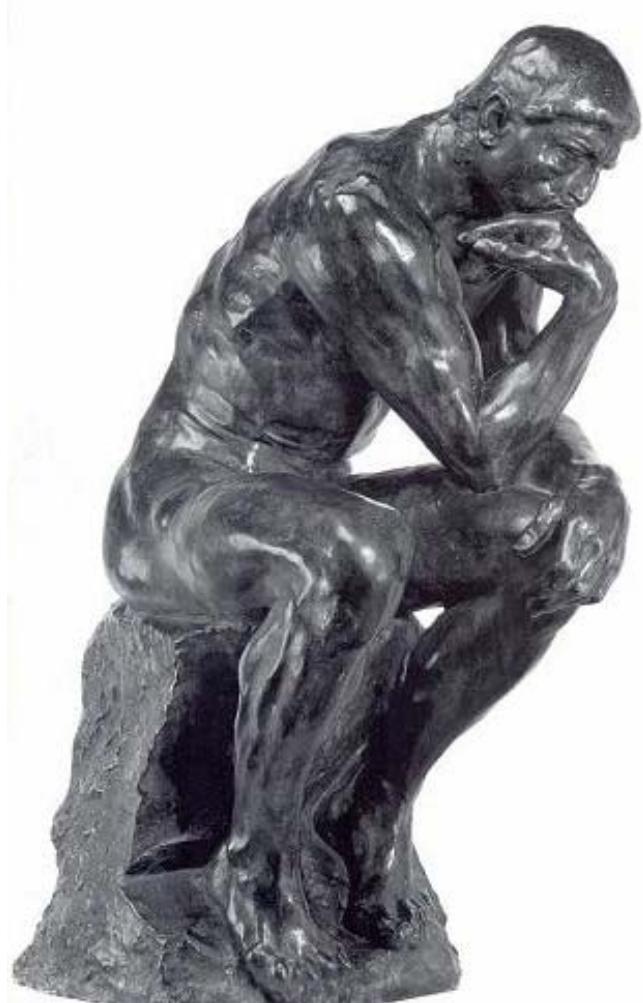
P. **Disposal.** Low-level waste disposal facilities shall meet the following requirements.

- (1) **Performance Objectives.** Low-level waste disposal facilities shall be sited, designed, operated, maintained, and closed so that a reasonable expectation exists that the following performance objectives will be met for waste disposed of after September 26, 1988:
 - (a) Dose to representative members of the public shall not exceed 25 mrem (0.25 mSv) in a year total effective dose equivalent from all exposure pathways, excluding the dose from radon and its progeny in air.
 - (b) Dose to representative members of the public via the air pathway shall not exceed 10 mrem (0.10 mSv) in a year total effective dose equivalent, excluding the dose from radon and its progeny.
 - (c) Release of radon shall be less than an average flux of 20 pCi/m²/s (0.74 Bq/m²/s) at the surface of the disposal facility.

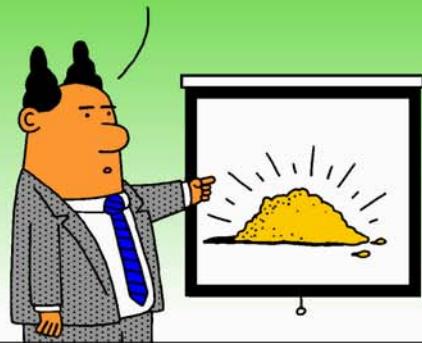
Uncertainty



Conscience



THE GOVERNMENT IS
NAGGING US TO GET
RID OF OUR DANGEROUS
RADIOACTIVE WASTE.



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ON A TOTALLY
DIFFERENT TOPIC,
I'M GIVING EACH OF
YOU A MOTIVATIONAL
PAPERWEIGHT THAT
SAYS, "NICE GOING."



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TRY TO AVOID
LICKING THEM.

